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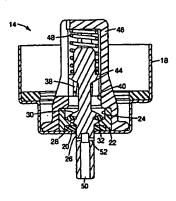
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(34) TIGH METERDIO VALVE POR A METERED DOSE DRIALIER PROVIDING CONSISTENT DELIVERY



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METERING VALVE FOR A METERED DOSE INHALER PROVIDING CONSISTENT DELIVERY

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Metering valves are a common means by which acrosob are dispensed from ol containers. Mesering valves are particularly useful for administering medicinal es that include a liquefied gas propellant and are delivered to a patient in an

nistering medicinal formulations, a door of formulation sufficient to produce the deniced physiological response is delivered to the patient. The proper revised amount of the formulation must be dispersed to the patient in cach successive dose. Thus, any dispensing system must be able to dispense doses of the medicinal flavoratorion accurately and reliably to belo assure the safety and efficacy of the

Meaning valves have been developed to provide control over the dispensing of medicinal serosol formulations. A metering valve may be used to regulate the volume of a medicinal formulation passing from a container to a metering chamber, which defines the nt of the formulation that will be dispensed as the next dose. Reliable and controllable flow of the medicinal formulation into the metering chamber may contrib to the accountry and/or procision of the metering of successive descript the fo Thus, reliable and controllable flow of the medicinal florostation into the metering chamber may improve performance of the mesoring valve and, therefore, may be highly desirable

Is some metering valves, the metering chamber fills with the medicinal formulation prior to the patient actualing the valve stem and thereby releasing the dose. The metaring chamber is refilled with formateries after dispensing one does so that the metering valve is mady to discharge the next dose. Consequently, the melating chamber contains formulation at all times except for the brief time during which the valve stem is depressed by the user to discharge a done. Also, the passageways through which the formulation must flow to reach the metering chamber are often currow and territoria. As a crasil, extering valves configured in this way have a number of disadvantages resulting in, for \cdot

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example, creatic dosing due to loss of prime. "Loss of prime" means the oc vapor or air voids in the metered volume, thereby leading to a shortfall in the volume of dose being metered by the valve. A principal cause of loss of prime is the presence of ess in the entry passersway or passersways through which formulation must pass to fill the metering chamber. Such restrictions can lead to flow disruption and thus also to the occurrence of water or air voids in the metering chamber.

Another phenomenon that can lead to creatic dusing is loss of dose. "Loss of duse" peans a change in the amount of suspended drug or excipient particles in a metered dose of flammatation, compared to the average composition of the bulk formulation in the container. A principal cause of loss of does is the settling of drug particles into, or their warment out of, sentricined regions of the metering valve such that the proper concentration of formulation cannot subsequently be obtained within the restricted region prior to dose delivery. For example, drug perticles may settle in a residual metering volume - any part of the metering valve bounded by a metering surface and that, when the metering valve is in the resting position, remains fluid filled but is not in substantially fire flowing communication with the bulk formulation.

In other metering valves, residual metering volume may be limited to some extent by designing the metering walve so that the metering chamber does not materialize unless and until the valve stem is actuated. However, even in these metering valves, a small residual metering wolume estima when the metering valve is at year because a small estandar gap exists between the valve stem and the metering valve body.

Actuation of these valve stems can be divided into a filling stage and a discharge stage. The filling stage begins as the valve store is depressed during accustion. The action of depressing the valve stem causes the formation of a transient metaring chamber, which is in Oxid communication with the residual metering walkage defined by the small assessing gap. As the velve stem is depressed, the transient portion of the metering chamber expands and formulation enters the matering chamber. As displacement of the valve st continues, a stage is reached at which filling of the transient metering chamber stape.

Eventually, displacement of the valve stem commes to the discharge stage, in which the meternal formulation is discharged. In these valves, a single actuation than causes capid filling of the transient metering chamber followed by discharge of the

the marketing to the parient. Generally, metared farmulation does not reside for any appreciable length of time in the metering chamber in these metering valves. However, nome formulation may resido in the residual measuring volume defined by the small annulus gap when the metering valve is at rest.

Some metering valves limit the bright of the annular gap, thereby reducing the maideal volume and limiting the amount of formulation that resides in the matering chamber between actuation events.

While a metering valve having a transient metering chamber provides advantages over other types of metering valves for the delivery of acrosed formulations, the flow of termeterion from the container to the texturing chamber may be disrupted. Disrupted flow of formulation refers to filling a metering chamber through one or more bottleneck regions of eignificantly restricted access. Flow through the bordeneck regions may be impeded sufficiently to give rise to substantially incomplete filling of the metering chamber, particularly under confitions typical of patient use. When this happens, formulati he delivered in inconsistent or inaccurate doses. Of course, all matering chamber inlets became similizantly restricted immediately prior to being scaled off during actuation. Disrupted flow, as just described, refers to flow severs during the majority of the filling stage of actuation.

Certain metering valves have been designed to improve the flow of formulation into the metering chamber. For example, some metering valves include angled spillway filling channels designed to limit disruption of the flow of formulation into the metering chamber. Less disrupted flow may decrease the likelihood and extent to which vapor or sir voids form in the metered volume and, therefore improve performance of the metering

Summary of the Invention

The present invention relates to a novel design for a metering valve that provides improved consistency of formulation delivery. The metering valve of the present invention includes a valve stem designed to (1) limit or eliminate the residual metering volume, thereby reducing the amount of formulation that resides in the metering chamber while the metering valve is at rest, and (2) limit restrictions on the free flow of formulation

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FEGS. 5 to 7 are enlarged cross-sectional views of the embodiment of an aerosal metering valve according to the present invention shown in Figure 1 in the resting position, the filling stage and the discharge stage, respectively.

FIG. 8 is an enlarged cross-sectional view of yet another embodies position.

FIG. 9 is an isometric, cut-away, enhanced view of a portion, i.e. in the vicinity of the measures easter, of the valve storp of the measure valve shown in FIG. 8.

FIG 10 is as incentric, cur-eway, cultured view of a portion, i.e. in the vicinity of the metering grades, of a further embodiment of a valve stem for war in an acrosol metering valve according to the present invention.

FIG. 11 is so colorged cross-sectional view of one conbodiment of a valve state according to the present invention.

FIG. 12 is an enlarged cross-sectional view of an alternative embodiment of a valve stem according to the present invention.

FIG. 13 is an enlarged cross-sectional view of another alternative embodiment of a valve stem according to the present invention.

PICS, 14 to 16 are enlarged cause-excitanal views of an alternative conhadiment of a mentring valve according to the present invention in the resting position, the filling range $\boldsymbol{\theta}$ and the discharge stage, respectively.

Detailed Description of the Invention

The following description is set flath in terms of an acrossi metering valve used to dispense an accord formulation from an accord container. However, the mettring valve and methods of the present invention have application to virtually any pressurized fluid coquiring delivery of an accurate, meteoral dose. In particular, the metering valves described bearinger could be dispensing medicinal across formulations.

When used to dispense medicinal acrosol formulations, a metaring valve according to the present invention may be used to education visually any account formulation of drug into a body cavity of a periom, such as the mouth, soos, emus, vagins, east, or onto the eyes or any skin som of the patient. However, the present invention is not limited to

into the metering chamber. Consequently, consistent delivery of formulation is obtained by strating the effects of loss of prime and loss of dose.

The present invention provides to accord metering valve that includes a valve healy and a valve stem that renerally defines a longitudinal axis and comprises a materia gasket configured to be able to form a transient, substantially finid-tight seal between the valve strm and a scaling purtion of the valve body. The valve stem includes a body portion including a metering surface, wherein the longitudinal sais and a plane tangential to at least a portion of the metering surface define an angle from about 2° to about 90°.

In another aspect, the present invention provides an across limetering valve including (a) a value body that includes a displease having walls that define an aperture (b) a metering stem that generally defines a central axis and also partially defines an interior space, the metering stem including a scaling portion, an inlet recess distal to the sealing portion, a metering surface distal to the inlet recess, and a discharge gashet distal to the metering surface, wherein the central axis and a plane tangential to at least a portion of the metering surface defines an angle from about 2° to about 90°; (c) a valve stem in slightle, scaling engagement with the sperture and including: (1) a scaling portion across a portion of the interior space from the inlet rocess of the metering stem; said scaling portion wising a metering gasker configured to be able to form a transient fluid-tight sliding scal with at least a portion of the metering stem scaling portion, (2) a metering surface configured to puberamially conform to the metering surface of the metering stem, (3) an inserior surface, (4) a discharge roccus in a portion of the interior surface.

Brief Description of the Drawings

FIG.1 is a cross-sectional view of a metered doss inhaler including an embodiment of the acrosol metering valve according to the present invention.

FIG. 2 is an enlarged cross-sectional view of an embodiment of another seroed metering valve according to the present invention in the resting position.

FIG. 3 is an enlarged cross-sectional view of the aerosol metering valve shown in FIG. 2 during the filling stage of valve stem actuation.

FIG. 4 is an entered cross-sectional view of the acrosol metering valve shown in FIG. 2 during the discharge stage of valve stem actuation.

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medicinal applications and may be used whorever a precise amount of material from a urized finid is to be delivered to a given region.

FIG. I shows an acrosol dispensing apparatus, generally designated as 10, that rates one embodiment of a metering valve 14 according to the present invention. 5 The top end of the metering valve 14 is crimped around the end of a conventional acrossi container 12, while a conventional discharge piece 16 is mounted around the bottom of the metering valve 14. Thus, across formulation is dispersed downwardly from the across container 12, through the metering valve 14, then through the discharge piece 16 where it is delivered to a patient. The discharge piece 16 directs the acrossol formulation toward the body cavity or skin area to which the formulation is to be delivered. For example, discharge piece 16 may be a mouthpiece that can be inserted into the patient's mouth, thereby providing and administration of the served formulation.

The aerosol-dispension device shown in FIG. 1 is merely one example of how a menaring valve according to the present invention can be incorporated into a dispersing appendus. Furthermore, the configuration of the discharge piece 16 depends upon the application for the serosol.

In many of the figures, a metaring valve or valve stem is thown in isolation for tion. The valve stems shown in isolation cary be combined with one or more additional components to form a metering valve. Such metering valves, as well as metering valves above in isolation in the figures, may be combined with one or more additional commonster to from an account dispensing device. It is understood that any mentionals fracture chown in a protection valve and/or valve stem embodiment may be combined with features shows in other embediments and/or incorporated appropriately within other embediments

Referring to FIG. 2 showing an embodiment of a metering valve 14 (in the resting position), the contaring valve 64 typically includes a housing 18 that serves to bosse the various components of the metering valve \$4. The top portion of the bouning \$8 strackes to the account container 12 (as abown in FIG.1). A valve body 22, typically scaled within the valve housing 18, in turn provides a housing for a valve sum 26. The valve body 22 includes an imprior surface 14 defining an internal chamber or cavity of the valve body.

The metering valve 14 typically includes a spring cage 46 that, together with the valve body 22, defines an interior chamber 38, a portion of which is occupied by a portion of the valve stem 24. One or more inless (not shown) provide open and uncestricted fluid communication between the interior chamber 38 and the aerosol container 13.

The valve stam 26 includes two portions, a body portion and a stam portion. The stam portion includes that portion of the valve stam that is consider the valve bouring 18 when the valve stam 26 is in the stating position above in FIG. 2. During actuation of the valve stam 26, however, the attem portion will be displaced inwardly with respect to the metering valve 14, as described more fully below, so that some of the stam portion will be transiently positioned inside the valve bearing 18. The stam portion includes a passageway 50 through which a metered dose of themselation is discharged, as will be described more fully below.

The body portion of the valve stem 26 is that partion that is positioned within the valve beasing 18 throughout actuation of the valve stem 26. The body portion of the valve stem 26 includes a metering surface 22 and a sealing surface 30.

The body person of the valve stem 26 is configured to have substantially the same shape as the surrounding wall of the valve body 22. Thus, as can be seen in the embodiment shown in FLG. 2, a submantial portion of the matering surface 28 of valve stem 26 rests in contact with the interior surface of the valve body 24 when the matering valve is in the resting position, thereby estimations the annular gap between the valve stem and valve body when the metering valve is in the resting position, and thus minimizing residual metering valves is in the resting position, and thus minimizing residual metering volume.

The metering valve may include a spring guide 44 mounted on the end of the valve stem body pertion opposite the stem portion and a spring 43 within the interior chamber 38 of the metering valve as shown in FIG. 1. The spring 43 through engagement with the spring guide biases the valve stem 25 toward the resting position. It will be appreciated by those stilled in the art that any exhibite means for biasing the valve stem 25 into the resting position, a.g. coil compression spring or a spring appropriately mounted external to the interior chamber, say to used in commercian with metering valves according to the present investion. The spring guide may be as integral part of the valve stem and/or

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34 is formed between the interior number of the valve body 24 and the metering number 25 of the valve stem 26. The volume of the metering chamber 34 increases as the valve stem is displaced small is reaches in filled-volume at the end of the filling stage.

Acrosol formulation criters the filling volume of the matering chamber 34 in the following manner. Formulation from the serveol container 12 pesses through the one or more index and into the interfew chamber 38 of the matering valve. From the interfew chamber 38, the formulation passes between the spring guide 44 and the metering gasket 32. Formulation flows around the proximal and of the valve stem 26 through a flow channel 43 between the valve stem 26 through a flow channel 43 between the valve stem 26 and the interior surface of the valve body 24 and extens the expending occuring chamber 34. The spring guide may be provided with converse the valve to the provided with converse the valve to the provided with converse the provided with the provided

Thus, as the valve scens 2.6 is moved from the nating position shown to FiG. 2 to the folling stage shown in FiG. 3, acrosed from the nation passes from the acrossol container 12 to the naturing chamber 34 immediately upon actuation of the valve stem 26. Formulation continues to fill the meaning chamber 34 until the meeting valve 14 reaches the filled triggs (not filterated). As will be described in more detail below, the flow of formulation into the metering chamber 34 may be afficied by the may be described by the metering nation of the valve stem 28 with respect to the entered beginnishmal axis of the valve stem.

At the end of the filling stage, the flow channel is cut off as the metering gasket contacts the sesting surface 40 of the walve body 22. The metering gasket forms a fluid-light, skiding smoker seal with the scaling surface (so can be seen in FRC. 4). The scaling surface 40 may include one or more structures designed to limit obscales of the extering gasket 32 as the metering pinket first contacts and then skides past the scaling surface 49. Simble structures include but are not limited to a counted citys, a bevoted citys, and a smooth angled transition from the interior surface of the valve body 24 to the scaling surface 40.

The dimensions of the valve body 22, valve stem 26 and other valve components determine the filted-volume of the metering chamber 34 in the completely filled position. FIG. 4 depicts the metering valve 14 in the discharge stage of actuation. In order to

discharge the meaning wave or or the meaning thempton in the meaning chamber 34, the valve atom 26 is further accusted to the position libertasted in FIG. 4. Those shilled in the erranged to include a pressure filling ring to described in the US Patern US 1,400,920, which is incorporated by reference herein.

The metering valve 14 sho includes at least two annulus gaskets, the disphagen 20 and the metering gasket 32. The disphagen 20 is positioned between the valve housing 12, the valve body 22 and the valve stem 26, as shown in FiG. 2. The disphagen 20 isolates the formulation in the serosel container 13 from the extrainer of the valve by forming two fluid tight seals: 1) on annulus sail between the disphagen 20 and the valve stem 26 where the valve stem actions out of the valve bousing, and 2) a compressive phase or face seal between the disphagen 20 and the valve bousing 18. The latter seal may be effected either with or without a sealing bend on either the valve body 22 or the housing

As shown in FIG. 2, the metering gester 32 is included in the valve stem 26, and forms two plants face scale with the body portion of the valve stem 26. The metering gestet may be either mechanically afficted onto the valves stem, modded onto the valve stem, or the valves stem may be manufactured using, for example, a two shot or co-mobiling process in which the valves stem sand metering gestet are co-modded so that a strong band (mechanical and/or chemical) can be achieved between the underlying portion of the valves stem and the metering gasket. As will be described in more detail below, the metering gasket 32 transferrly inolates the formstation in a metering chamber 34 (which is formed during actuation) from the servesol container 12 (as can be best seem in Fig. 4) and thus provides a means for terminating the flow of formulation from the servesol container 12 to the metering chamber 34 during actuation of the valve stem 26.

Operation of the metering valve shown in FIG. 2 is illustrated in FIGS. 3 and 4.

The figures illustrate the stages of operation of the metering valve 14 and the corresponding relative positions of the valve components as a patient actuates the valve stars 16, thereby releasing a dose of acrossi formulation. FIG. 3 shows the metering valve 14 in the filting stage and FIG. 4 shows the metering valve 14 in the discharge stage.

As can be seen in FIO. 3 during the filling stage of actuation, the valve stem 26 has been displaced inventily into the interior chember 38 against the compressive force of the spring 48. As the valve stem 26 is displaced invently, the proximal end of the stem portion of the valve stem 26 enters the valve housing 18. As a result, a metering chamber

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art will realize that the distance traveled by the valve sizes 26 between the start of the filled stage and FRG. 4 will result in on expansion of the nestering chamber 34 without increasing the metered does. The actus travel ensures that the metering gaster 32 is scaled against the scaling surface 40 before the one or more side holes 52 enter the metering chamber 34. As the valve stem 26 is fully scanned, the one or more side holes 32 of the discharge passageway 50 pass through the disphragm 20 and come into fluid communication with the metering chamber 34. The fluid communication thus established allows the across formulation within the sentering chamber 34 to be released into the one or more side holes 52 and the formulation who passes through the discharge passageway 50, thereby delivering the metered does of across formulation to the potiests or other desired area.

During the discharge of the serveol formulation from the metering elember 34 as thown in FIG. 4, the restering gasket 32 continues to prevent the passage of additional bells formulation from the serveol container 12 to the metering chamber 34, with allowance made for the dimensional tolerances of the valve components. After the does of serveol firmulation is discharged, the patient releases the valve stem 26, which returns to its original resting position depicted in FIG. 2 by at least the bissing action of the spring

The successive stages of valve stem actuation, as exemptarily depicted in FRGS. 3 and 4, are all accomplished during the brief duration of actuation of the valve stem. Accordingly, formation, filling and emptying of the sectoring chamber occurs regisfly. At most, only a very small percentage of a dose of formulation resides in the metaring chamber between actuations. In score embodiments, the metaring chamber may not exist at all in the cesting state - the residual metaring volume may be zero - so that no formulation can reside in the metaring chamber between actuations. Descarse the stages of valve stem actuations occur regisfly, the metaring chamber is full of formulation only the shrief momenta immediately prior to discharge of the fluxualistics from the metaring chamber.

FIGS. 3 to 7 dilustrants another embodiment of a matering valve 14 in its resting position, during filling stage and discharge stage of actuation. This embodiment provides an example in which the spring guide 44 and valve stam 26 are formed as a single cleaness, he this embodiment, the part of the matering surface 28 located adjacent to the imprison

between the metaring nurher and sealing surface has no significant portion aligned parallel or nearly parallel to the stem axis. Furthermore, the metaring nurhers 28 is configured to have unbeautistly the same shape as the ammuniting wall of the valve body 12. Thus, in this embodiment, substantially the complete purition of the metaring surface 126 of the valve stem 26 rests in contact with the interior curface of the valve body 24 when the metaring valve is in the resting position (as shown in FiG. 5), thereby minimizing, if not substantially eliminating, any residual metaring volume.

Abo, in this embodiment the pert of the scaling nurface 30 located adjacent to the interface between the metering surface and scaling surface has no significant portion aligned parallel or nearly parallel to the stem axis. This facilitates free-flowing communication between the both formulation and formulation through this the interior chamber 38, in particular in the vicinity of the body portion of the valve stem 26 and the internal chamber or cavity of the valve body 22 defined by the interior surface 24 of the valve body wall, when the metring valve is to the resting position.

During actuation of the metering valve 14 (as illustrated in FIGS. 6 and 7) – the operation of which is the same as that described for the embodiment illustrated in FIG. 2 to 4. five flow of formulation during the filling stage (FIG. 6) into the metering chamber 34 formed upon actuation is also enhanced, as discussed in more detail below, due to the desirable configuration of the metering surface 24 and/or scaling surface 30 of the body portion of the valve strap 25.

FIG. 8 illustrates a further embodiment of a metering valve 14 in its resting position. This embodiment provides an extemple in which the spring guide 44 is formed of two parts, a spring guide seem 44° and a spring guide cap 44°, wherein the valves and apring guide stem are formed as a single element and the spring guide cap is formed as a sprease defences, which is subsequently affixed onto the spring guide cap.

In this embodimens the part of the metering surface 18 located adjacent to the interface between the metering surface and the stating surface 30 is condigured to have subcrassially no portion aligned parallel or nearly parallel to the stem acts. Purthermore, the metering surface 18 is configured to have essentially the some shape as the surrounding wall of the valve body 21. Thus, in this embodiment, essentially the completes portion of the metering surface 18 of the body portion of valve stem 24 retain in contact with the

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During actuation of the metering valve 14 (not illustrated) shown in FIG. 8 – the operation of which is the sums as that described for the embodiment illustrated to PRG. 2 to 4 - fires flow of formatsion during the filling stage into the metering chamber 34 formed upon actuation is enhanced, as discoused in more detail below, the to the desirable configuration of the metering surface 28 and/or scaling surface 30 of the body portion of the valve stage 25.

As mentioned above, the configurations of the valve body 23, valve stem 26 and in some cases other valve components influence five flow of formulation and the presence of residuel menting volume, when the menting valve is in its resting position as well as the flow of formulation into the sectoring chamber 24 when the valve stem is actuated.

For example, when the metering portion (a portion that, in part, bounds the neturing chamber formed upon actuation) of the valve body is configured to substantially conform to the metering surface of the valve stem, when the metering valve is in its resting position, the presence of residual metering volume is minimized. Under the term "metering parties of the valve body is configured to substantially conform to the m surface of the valve stem", it is desirably understood that a significant portion (e.g. \geq 15%) of the contrast purples of the valve stars reats in connect with the interior surface of the valve body when the menuing valve is in the resting position. The residual metering volume may be further minimized, by coefficiency the metering portion of the valve body to executably conform or to conform to the metaring surface of the valve stem when the value is at cres. Under the term "meterine portion of the valve body is confirmed to examisely conform or to conform to the metaring surface of the valve stem", it is desirably enderstood that automobilly the complete partion (s.g. ≥ 90 %) or executivilly the complete portion (e.g. ≥ 95% or more desirably ≥ 97.5 %), respectively, of the metering surface of the valve gaza cests in connect with the interior surface of the valve body when the meaning valve is in the resting position.

As described above, fine flowing of formscholor in the velve in its rest position may be further describly influenced, by configuring the metaring surface of the body portion of the valve stars, such that oo significant portion (e.g. $\le 5\%$ or more describly $\le 2.5\%$), more animally no automatical portion (e.g. $\le 2\%$ or more describely $\le 1\%$), or most animally no portion of the metaring surface adjacent to the interface between the

interior surface of the valve body 24 when the metering valve is in the resting position (as shown in FIG. 8), thereby substantially eliminating any residual metering volume. In this embodiment the part of the scaling surface 30 located adjacent to the interface between the senting surface 28 end scaling surface is also configured to have steministly no portion aligned perallel to the stem sais, in particular adjacent to the interface between the metering surface 28 and the scaling surface. This again enhances from-flowing communication between the bulk forcumbation and forcumbation within the interior chamber 13, in particular in the vicinity of the body portion of the valve stem 26 and the internal chamber or cervity of the walve body defined by the interior surface 24 of the valve body well, when the metering valve is in the resting position.

As can be appreciated from FIG. 8, the metering gashes 32 of this embodie substantially triangular in chaps. The inner surface of the metering gasket 32 is typically affixed to the respective underlying portion of the valve stem 26 as a result of a molding (e.g. molding the gasket onto a metal valve stem) or, more desirably a co-molding. manufacturing process used to produce the valve stem. As mentioned above, the use of comolding processes allows the provision of a strong bond between the interface of the ncturing gasket and the underlying portion of the valve atom. To enhance bonding and/or to further ensure mechanical support and strength, the underlying portion of the valve 26 may be provided with key(s) or geometrical feature(s) 33, which facilitate or enhance mechanical anchorage of the molded or co-molded metering gasket 31, For better understanding, FIG. 9 illustrates an isometric, cut-away, enlarged view of a portion, i.e. in the vicinity of the metering gustest, of the metering valve shown in FEG. B. As can be seen the portion of the valve atom 26 underlying the inner surface of the metering grathet 32 is provided with keys 33 in the form of a series of alternating triangular teeth, which may optionally be slightly undercut as shown. As will be appreciated the form of the key(s) may be of any mitable from, desirably a non-recutant from for case in manufacturing (a.g. using injection moulding tooling with an axial direction of tool half split movement). which facilitate or enhance anchorage of the meterless gaskes. Snitable forms include Lstuped extensions, desirably alternatively up and down, T-shaped extensions, as surely fings or as exemplified in FIG. 10 an ansular finnes 33 provided with holes or elongated perforations 33°.

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naturing nurface and the scaling surface of the body portion of the valve body is aligned parallel or nearly parallel on the stem axis (i.e., with a very small stage θ_i , θ_i , θ_i or θ_i). Also, free-flowing communication between the bulk formulation and formulation within the interior chamber, in particular in the vicinity of the body portion of the valve stem and the intermal chamber or cavity of the valve body defined by the interior serface of the valve body wall, when the metering valve is in the resting position may be enhanced by cortain configurations of the scaling surface of the body portion of the valve stem. In particular, it may be destrable to configure the scaling surface of the body portion of the valve stem. In particular, it may be destrable to configure the scaling surface of the body portion of the valve stem. In particular, it may be destrable to configure the scaling curface of the body portion of the valve stem, the particular portion (e.g. ≤ 2 % or more destrably ≤ 2.5 %), more suitably no substantial portion (e.g. ≤ 2 % or more destrably ≤ 1 %), it must suitably no portion of the scaling surface adjacent to the interface between the metering surfaces and the scaling surface of the body portion of the valve body is aligned parallel or nearly parallel to the stems as in

As mentioned above, the flow of forembation into the metering chamber during actuation may be affected by the major described by the metering surface of the valve stem with respect to the counts longitudinal axis of the valve stem. For example, the valve stem 26 may define a control longitudinal axis 60, as shown in FiG. 11. An engire θ_0 , may be defined by the intersection of a plane 62 tengential to a major portion of the metering surface 128 of the valve stem and the control axis 60, he some embodiments with complex geometries, engire θ_0 , sury be defined by the intersection of the control axis 60 and a plane temperated with a minor control of the metering surface.

All the being equal and assuming that the velve body is configured to information conform to the valve stam, a larger θ_0 , results in a wider filling gap for a given displacement of the valve stam during actuation of the metering point, a larger value of displacement of the state of the processing displacement distance to the metering point, a larger value of θ_0 , generally ablove the valves stam and the metering valve to be abortor. The shape of the metering services 23 shown in FIG. 13 allows the use of a particular angle θ_0 in a shorter metering valve. A simpler metering surface, such as that shown in FIG. 11, may require less dimensional control in order to manufacture the valves stam and valve body that substantially conform to one another and thereby limit or eliminate residual metering valves the metering valve is at real.

Suinble values for angle Θ_n in valve stome according to the present invention are from about 7° to about 90°. Within this range a minimum angle of about 10° is more desirable, about 20° even more desirable and about 30° most desirable. A maximum angle of about 80° is more desirable and about 60° most desirable and about 60° most desirable.

To limit the potential of areas of restricted flow within the matering clamber and thus enhanced free flow of formulation into the metering clamber, the metering surface is desirably configured to have on significant portion (e.g. ≤ 5 % or more desirably ≤ 1 %), or most minthly no substantial portion (e.g. ≤ 2 % or more desirably ≤ 1 %), or most minthly no portion thereof sligned possible or nearly parallel to the stem axis.

As can be seen in the exemplary embodiments shown in FIGS. 2, 5 and 8, the body portion of the valve stem typically includes a section edjacent to the stem portion, which is aligned parallel or nearly parallel to the stem axis. This section facilitates the passage of the valve stem through the opening of the valve bossing and/or the disphragm. Because this section is edjacent to the stem portion and at the distal end of the metering chamber formed upon actuation (as can be appreciated for example in FIG 6), a parallel or nearly parallel alignment of this section of body portion does not restrict the flow into the metring chamber.

As can be best seen in FIGS 11 to 13 showing exemplary valve stems, the metaring surface 28 is typically that surface of the section of the body portion located between the section of the body portion comprising the scaling surface 30 and the section of the body portion adjacents to the stem portion being sligned parallel or nearly parallel to the stem axis. The circumferential interface or boundary of the metaring surface and the scaling surface, being located on the outer surface of the metaring spatch; is typically understood to be the annulus of widest transverse cross section of the metaring spatch. Do embodiments, which is accordance to the aftersaid definition would have an interface or boundary having a portion passible to the longitudinal axis of the stem, the interface or boundary is understood in this case to be the annulus at the distall end of the parallel portion (i.e. the cent inverted the stem portion). As can be appreciated from FIGS. 11 to 13, if the valve stem includes a momented or integral spring guide 44, the scaling surface 30

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relatively simple geometry, such as the valve stem shows in FIG. 11, a majority of the metering surface 12 may define the plane 61 stand to define angle 6.— Alternatively, the metering surface 12 may be irregulat, such as in shown in FIGS. 12 and 13, and only a portion of the metering surface may be used to define the plane 63. Additionally, irregulation in the metering surface 22 may be non-opeometrical and still provide a satisface configuration for valve storn 24 seconding to the present investions.

Thus, the particular geometry of the activing nurther 28 is not critical so long as (1) argic 4₆, can be defined as described herein, (2) the interior surther 24 of the valve body 21 is configured to nobstantially conform to the geometry of the metring surther 28. These flexture contribute to limiting or eliminating residual metring volume when the metring valve is at sex and facilities the reduction of restriction of the flow of formabilion to the metring chumber. Furthermore, it may be advantageous for limiting or eliminating residual metring values that no significant portion of the metring surface and/or the scaling surface adjacent to the interface between the metring surface and the scaling surface adjacent to the interface between the metring surface may be configured to have no significant portion aligned particle or overly parallel to the some six. This may committee to limiting the formation of areas of restricted flow within the metring chamber and thus entireing on the first flow of formulation into the metring chamber were though the instruction surface 24 of the valve body 22 substantially conforms to the geometry of the metring surface 28.

Simple geometries for the metering surface 12 and the interior surface 24 of the waive body cary provide certain manufacturing advantages. For example, valve stress having complete 560° continual symmetry require no rotational alignment during valve assembly. Simple stapes such as comes might also confer certain performance advantages. • For example, simple stapes such as comes might also confer certain performance advantages. • For example, simple stapes may endous problems with deposition of dwag or with formalization flow discontinuities at simples odpes. However, more complex geometries also see authorities for valve mores 26 according to the present invention. For example, some embodiments may include valve stress loving multiple engles, each as those shown in FGS. 12 and 13.

ends at the interface or boundary between the surface of the body portion of the valve stem and the surface of the spring guide.

The flow of firemetration into the metering chamber during actuation as well as free flow of farmatistics when the metering valve is at rest any also be afficient by the angle described by the sexting surface of the valve stem with respect to the contral longinedinal axis of the valve stem. Referring to FIG. 11, an engle 0, may be defined by the intersection of a place 64 tangential to a major portion of the scaling nerface 30 of the valve stem and the contral axis 60. In some embodiments with complex geometries, angle 0, cary be defined by the intersection of the central axis 60 and a plane tangential with a minor portion of the scaling surface 30. Typical values for engls 0, in valve stems may be from about 30° to 90°. Within this range, a minimum angle of about 45° is more destrable and about 50° most desirable, A maximum angle of about 85° is more desirable and about 50° most desirable. A maximum angle of about 85° is more desirable and

Metering varies having an angle 0, in the ranges described may have a meaning portion - a portion that, in part, bounds the metering chamber - that one generally be described as comical in shape with a cross-sectional area of the proximal portion of the cone. In some embodiments, the transverse cross-sectional area of the distal portion of the cone. In some embodiments, the transverse cross-sectional area of the valve stem body at the metering and sealing surface interface may be about 4% greater than the transverse cross-sectional area of the distal end (i.e. towards the same portion of the valve stem) of the valve stem body. In other exchodiments, the transverse cross-sectional area of the valve stem body at the metering and scaling surface interface may be at least about 20% greater than the transverse cross-sectional area of the distal end of the valve stem body. In still other embodiments, the transverse cross-sectional area of the distal end of the valve stem body at the metering and scaling surface interface may be at least about 60% greater than the transverse cross-sectional area of the valve stem body at the metering actional streat of the valve stem body at the metering sectional area of the valve stem body.

In certain embediments having a generally conical metering portion, the interior surface of the valve body maintains a generally conical form from the disphragm to the valve body scaling partics.

The metering surface 28 of the valve sum 26 may be of any missbin configuration and still define the plane 62 used to define angle 6_m. For example, in a valve sum having

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The embodiments described above are provided in the context of metering valves having a displaceable valve atmn summended by a valve body. However, one size may design a metering valve in which the displaceable valve size atmostered the valve body. Such an embodiment is shown in FIG. 14-16. FIG. 14 shows the combodiment in the setting stags, FIG. 15 shown the same embodiment in the filling stage, and FIG. 16 shows the same embodiment in the discharge stage.

The metering valve 116 of FIG. 14 includes a bossing 118 that serves to bosse the vertous components of the metering valve 114. The top portion of the bossing 118 smaches to the servesol container as shown with respect to an alternative embodiment in FIG.1. A valve body 122 is ested within the valve housing 118 and in turn provides a bossing for a valve stem 126.

The mettering valve 114 includes a metering body 124 that, together with the valve body 122, defines an interior chamber 138 that is purefully occupied by a portion of the valve stem 126. At less one infer (not shown) provides open and unrestricted fluid communication between the interior chamber 138 and the ball: formulation stored in the across containing.

In the embodiment shown in FIGS, 14-16, the metering body includes a stem portion 133 that generally defines a central axis 160. The stem portion 133 of the metering body 124 includes an index toxers 113, a scaling surface 113, a sectoring surface 114, and a discharge gacket 117. The discharge gacket 117 forms a didning send with the inserior surface of the valve team 130 and includes the interior chamber 138 from the casteries of the valve when the nearting valve is in the stating position.

A portion of the valve stem 125 resides within the bousing 119 throughout artention. Another portion of the valve stem 125 resides cotticle the valve housing \$18
25 when the valve stem 125 is to the resting positions shown in FIG. 14. During estantian of the valve stem 126, a portion of the valve stem 125 that resides outside the housing 118 will be displaced inwardly with respect to the matering valve 114 so that it will be translutedly positioned circle the valve housing 118.

The valve atom 126 of the matering valve 114 shown in FIGS. 14-16 includes a matering perhet 131. The matering gentes 132 from a planes fines seed with the valve stem 175 and in positioned so that it can from a disting atomate and with the seating

surface 113 of the stem portion 123 of the metering body 124. The valve stem 126 also includes a metering emphor 128, a discharge recess 136, and a discharge passageway 150. The discharge passageway 150 may be in finid communication with a discharge piece 152.

FIG. 13 shows the metering walve of FIG. 14 in the filling stage of actuation. The valve atom 126 is shown partially actuated - it has been displaced inward with respect to the saem person 123 of the metering body 124 and, therefore, also with respect to the entire metering walve. Thus, the valve atom metering surface 128 has been drawn a way from the metering surface 116 of the metering body. The resulting space defines, in part, the metering chamber 134. Formulation is permitted to flow from the interior chamber 134, through the passage formed between the metering peaket 132 and the inlet roceas 112, and into the metering observed 134.

In operation, the valve mean \$26 is further actuated to the filled sings (not shown). In the filled sings, the metering gashet \$32 eventually contacts the scaling surface \$135 and forms a finit-cipit sliding scal. This scal isolates the metering chamber \$134 from the interior chamber \$38 and sings the flow of formulation into the metering chamber \$34.

FIG. 16 shows the valve sum 126 actuated to the discharge stage. The valve stems 126 is shown actuated sufficiently so that the discharge racess 136 allows metered formulation to flow from the metering chumber 134, around the discharge gasket 117, and into the discharge passageway 150, from which the metered does of formulation may be delivered to a patient. The metering gasket 137 malmains the tilding seal with the senting surface 113, thereby continuing to isolate formulation in the interior chamber 138 from the carrier of fits valve.

FIG. 16 sho shows the determination of angle θ_m in the illustrated embodiment. As with the embodiments shown above, angle θ_m is defined by the central skil (shown as 162 in FIG. 16) tangential to at least a portion of the metering surface. In this embodiment, the plane such of define angle θ_m is tangential to at least a portion of the metering surface it is tangential to at least a portion of the metering surface it is of the stem portion of the metering body 123.

Because style 8, is defined, in part, by a plane tangential to a portion of the metaring surface 116 of the stem portion of the metaring body 123, the distal portion of the metaring body - the portion near the discharge gaskst 117 - will have a transverse cross-sectional area of the prezimal portion of the

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themostropic tiquid crystalline polymens (LCPa), polypropylena, high density polypropylena, chylena-curathorocchylena copolypers (ETPE), polypringidians diffuorida (PVDF) and mixtures themod. The material may include typical fillers, each as fibers (e.g. glan, mixend or carbon fibers), minemals (e.g. CHCOs), graphist or carbon, which may enthrone structural robustness. PyS- and PST- containing assertable desirably incorporate fillers, e.g. made of glassifier, while the other polymer-containing materials are desirably free of fillers. For the provision of valve stress showing desirable resistance to mechanical and/or thermal stress or deformation, the polymer is desirably selected from the group consisting of polyary/scherketones, such as polyetherscherketone, thermotropic liquid crystalline polymers, polymetrylymentons, polyphenylene sulfide and mixtures thereof.

The metering gasket is typically elastomeric and may be made of a material comprising a thermophettic elastomer or a thermoset elastomer.

Various classes of exitable thermostastic electroners include polyecter robbers. rolywethane rubbers, eshylene vinyl acessus subber, stysson butadiene rubber, copolyeste: thermophysic elastopiers, copolyester other thermophysic elastomers, olefinic hermoplastic elastomers, polyester amide thermoplastic elastomers, polyether amide thermoplastic elastomers, copolyamide thermoplastic elastomers and mixtures thereof. Exemples of eletimic thermophystic electroners are described in WO 92/11190, which is incorporated berein by reference, and include block corpolyment of ethylene with monogen selected from but I ema, here I ema and oct-I ema. Other examples of anitable alefinic thermosterric electroners are described in WO 99/20664, which is incorporated berrin by reference, and in US 5703187 (Dow). Streets-calvidens-butadiens-streets construers and blends, such as those described in WO 93/22221 and WO 93/03984, both of which are incorporated herein by reference, as well as styreno-callyfemo-propylenostyrens copolymens are suitable thermophesia classumers. An example of a polyether smide thermophonic elementer in PEBAX (Attribut), which is a polyether-block-copolyamids. Compositions comprising a mixture of inter-dispersed relative bard and relative suff durantes may also be comboyed as suitable thermorphysis chast Examples of such mirrors correspondence include SANTOPRENE (Advanced Electro Systems) which has therefore EPDM dispersed in a polyoletin matrix or ESTANE (Novece) which is a polymer of argumented polycuter continues with a mixture of

matering body 123 - that portion near the inlet recess 112. In some embediments, the transverse cross-sectional sers of the distal end of the metering body may be about 4% greater than the transverse cross-sectional sers of the proximal end of the metering body, in other embediments, the transverse cross-sectional area of the distal cross of the metering body may be at least about 20% greater than the transverse cross-sectional area of the proximal end of the metering body. In still other embediments, the transverse cross-sectional area of the fitted end of the metering body may be at least about 60% greater than the transverse cross-sectional area of the fitted end of the metering body.

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As with the embodiments described above, the metering surface 116 of the stem portion of the metering body 123 may substantially conform to the shape and dimensions of the metering parties of the valve stem 128. Thus, a metering valve couploying this during may limit or own eliminate residual metering volume between the metering body metering surface 116 and the valve stem metering surface 128 when the metering valve is in the resting position.

The design of the metering surfaces according to the present invention may countilum, along with other expects of metering valve or valve term design, to improve the flow of formalistics through the metering valve during actuation. Accordingly, the designs of the present invention may be used in conjunction with general metering valve designs of the present invention may be used in conjunction with general metering valve designs may include one or more additional features of the valve stem, valve body, or any other portion of the metering valve designed to improve performance of the metering valve.

Such additional design features may improve metering valve performance by improving performance permeters techning but not limited to formulation flow from the seroest container to the necturing classibler thring actuation and consistency of formulation

For embodiments incheding a co-molded metering gasket, the non-metering-gasket portion of the valve stem (methoding the stem portion, most of the body portion and possibly the spring gaide or a portion thereof), termed as the clongsto stem element in the following, is desirably made of a material competiting a polymer. Solitable polymers inchede sectal, nyton, polyester (PE), in periodal polybertylene tempholastus (PBT), polymentylepentene (PAIT), p

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crystalline and rubbery nanophases. Other mixtures include obelinis thermoplastic/rubber blands and polyvinyl chloride/rubber blands. Other possibilities include single-phase melt-processable nubbers and incorners.

Preferred thermoses elastomers include thermoses ethyleno-propyleno-dicase empolymer (EPDM), acrytonin'ilo-bamdiene copolymer (Nitrile robber), isobutyleno-imperess expolymer (Baryl robber), hisdagastied isobutyleno-imperes expolymer (in particular Chlorobutyl robber and Bromobutyl robber), polycidamperes (Pooperes), and mixtures thereof, with EPDM, mixture robber and buryl robber being more preferred. EPDM and withile robber cover more preferred and EPDM most preferred.

Combinations of co-motded meaning gathers made of materials comprising thermoset EPDM, thinks rubber, burnly mibber, chlumbarly nibber, brunnohurpl mibber and/or occpress, in particular EPDM, with clongras atom elements made of materials comprising a PAEK, LCP, FPS and/or PAO polymer provide walve stems having perticularly solventageous properties in eigent to mechanical sadder chemical stress resistance in dispersing valves (e.g. metered dose dispensing valves) for delivery of medicinal seroes formulations. It is to be understood that each of the possible M metering gasket/chongras stem element material combinations is individually disclosed bers. Valve stems comprising chongras stem elements made of materials comprising PAEK, more particularly polyetherethertectors, and co-modded metering gasket(s) made of materials comprising the elements of the properties and the medicinal seroes formulations, to particular medicinal seroes formulations comprising themses EPDM show superior structural seroes formulations comprising liqualized properties threads and/or HFA 227, more particularly such formulations comprising additionally ethenol.

The valve stem may be manufactured by an over-molding or an under-molding 25 unnexts.

The former method comprises the steps of:

a) providing a first mold shape;

b) mobiling a first material comprising a polymer to face the changate stem

 c) providing a second mold shape containing at least in part the changes term chemical, and 5

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 d) molding a second material to from the metering gashet, such that the metering gashet is co-molded with at least a portion of the changate stem element.
 The second, under-molding, method comprises the steps of:
 a) providing a second mold stape;

b) mobiling a second material to form the metering grather, c) providing a first model abupe undurlying at least to part the metering grather, and d) trackling a first material comprising a polymer to form the clongate stem element having the metering grather to-molded with as least a portion of said clongute stem

For the rate of consistency in the two shamstive methods, the wording "flrst" mold shape and "first" material are used here in connection with steps relating to the molding of the clongate stem clement, while the wording "accound" motoid shape and "accound" material are used in connection with steps relating to molding of the metering gaster, regardless of the sequential order of the process steps. For molding of the clongate stem chrones and/or molding of the matering gaster, the preferred method of molding is injection molting.

It will be appreciated by those skilled in the set that respective mold shapes will be provided as to allow the provision of the particular form of changes stem alconest and metering gashes needed for the use of the valve stem in the particular dispensing valve. The method may involve a molded component being removed from its mold and then positioned appropriately is another mold form for the medding of the other component. Alternatively the method may involve a single, repositionable or form-changeable mold, in which upon molding of a component, the mold is se-positioned or changed to provide the appropriate form them there for molding of the other component.

For valve status which include a matering gaster made of a material comprising a thermost clustomer, the material used in the molding steps, more particularly injection molding steps, the forming seal cleaneds ("the second material") desirably comprises a thermosetable clustomer. A thermosetable elestomer is understood here to mean a material (more particularly an injection moldiable material) comprising a polymer moleculus beving at least one double bond, in particular polymer moleculus having althous groups,

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optimal curing conditions, curing agents, etc. depend on the particular thermosentable classimors being motived and possibly also on the overall dimensions, aims another floran of the particular metering gadest being mobiled. In regard to process efficiency, it may be desirable to use higher temperatures over thorter times to achieve rapid turnover through the mobiling tools.

In both methods after the coming step and the removing of the final model shape, it may be desirable to perform an additional thermal treatment step, for example to substantially complete cross-linking another to optimize physical properties of the thus formed metering gashet. This thermal treatment step may involve bearing between 110 and 200°C for replacify a longer time period than the curing step, e.g. over a time period of 0.5 to 24 hours.

Various modifications and alterestions to this invention will become apparent to those skilled to the set without departing fitnes the scope and spirit of this invention. It should be understood that this invention is not intended to be unduly limited by the Ulestrative embodiments and examples set forth bench and that such examples and embodiments are presented by way of example only with the scope of the invention intended to be limited only by the claims set forth bench as follows.

more particularly pendant afteno groups, which provides sizes across which cross-times can be formed upon a curing process allowing the provision of a thermoset electromer.

For example, thermosentable shatomers used to provide thermoses EPDM (cdzykmo-propykmo-diene terpolymer) and mirrile rubber (an acrytoniarile-baradiene copolymer) typically comprise a polymerized diene, which provides alterns groups in the polymer for cruss-linking. Butyl rubber is typically made from a ploymer comprising polyisobatene with a minor proportion of isopense to provide alterns groups the cruss-linking, while balogenased butyl rubber, e.g. CIDR and BIDR, is typically made by halogenation of the respective polymer prior to caring. Halogenation does not reach in a loss of unsaturation, and cross-linking is typically achieved using magnesium cuide solder zinc cuide, prefundly zinc cuide, resulting in the elimination of the respective metal halde. Similarly Neoprene is typically cross-linked via the elimination of metal chlorids from polychlosopene using magnesium cuide and/or zinc cuide optionally with an allydication.

In the methods of manufacturing, subscapent to the step of molding (more particular injection molding) a second material comprising a thermosestable classomer, the methods would include a step of curing said accord material. The curing step, which is typically performed directly after the step of molding of the second material, may be performed at appropriate time after said molding and prior to remove the final mold shape in the process.

The curing process is desirably performed such that at least a majority of the crosslink bonds is formed. Processes for cross-linking see well known and two common types include sulfur-curing, which typically kwolves sulfur donor molecules to provide polymilified bridges, and percuide curing, in which percuide molecules provide a source of free radicals allowing alkiene or pendant alknes groups to form a bridge. Percuide curing is typically the preferred method of curing, in order to provide materials from which a minimum of hamful extractables could potentially be leached. In percuide curing to provide a halogenated buyly rubber, such as CUR and SIML, a co-valentizing agent, such as PUP"—phenylene-dimaleimids, in often used to achieve adequate cross-linking. Curing processes typically also involve thermal treating, ag. heating between 110 and 200°C for a minute or more, allowing at least a majority of the cross-link-bonds to be founded. The

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What is Claimed is:

- 1. An acrosol metering valve comprising:
 - (a) a valve stom that generally defines a longitudinal axis and comprises:
- (1) a body pertion comprising a metering surface, wherein the longitudinal sais and a plane tempential to at least a portion of the metering surface define an angle from about 2" to about 90", and
 - (2) a stom portion comprising a disabeten passageway, and;
 - (3) a mestring gashet
 - (b) a valve body comprising:
 - (1) a body wall that comprises a scaling portion,
 - (2) an internal chamber defined at least in part by the body wall and comprising a matering portion configured to autostantially conform to the matering surface of the valve arm, and
- (c) a disphragm having walls that define an aperture in slidable, scaling engagement with the stem portion of the valve stem; and wherein the containing gusten is configured to be able to form a transient, authorized bind-eight scale between the valve stem and the scaling portion of the body wall.
- 20 2. An acrosol metering valve according to claim 1, wherein the body portion of the valve stem comprises a scaling surface edjacent to the metering surface and distinct to the stem portion of the valve stem and wherein said scaling surface and the metering surface form a circumferential interface on the outer surface of the metering gentlet.
- 3. An acrosed metering valve according to claim 2, wherein no significant portion of the metering surface and/or the scaling surface of the valve stem edjacent to the interface between the metering surface and the sealing curface is aligned parallel or occurry parallel to the longitudinal scale.

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4. An accross measuring valve according to claim 2 or 3, wherein the longitudinal axis and a plane temperature as least a portion of the scaling surface define an angle from about 10° to about 90°.

- 5 f. An acrossol metazing valves according to any preceding chaim, wherein the metering's garket is configured to be able to form a undetentially fluid-tight, sliding and with at least a portion of the scaling portion of the body wall.
 - 6. An acrosol metering valve comprising:
 - (a) a valve body that comprises a displaragin having walls that define an aperiture,
 (b) a metering stem that generally defines a longitudinal axis and also pertially defines an interior space, the metering stem comprising a sealing portion, an index recess distal to the sealing portion, a metering surface distal to the inlet recess ad displaraging portion, a metering surface distal to the inlet meters and a displaraging meters distal to the metering surface, wherein the central satis and a phone temperature of the sealing portion of the metering surface defines an another from about 2° to about 90°:
 - (c) a valve sum in slidable, scatting engagement with the operature and comprising: (1) a scatting portion across a portion of the interior space from the infet
 - trees of the meaning states, said scaling portion comprising a metering gradual configuration to be able to form a transient fluid-right between the valve stems and the scaling portion of the naturing stem.
 - (2) a metering surface configured to substantially conform to the metering surface of the metering stam,
 - (3) en interior surface.
 - (4) a discharge recess in a portion of the interior surface, and
 - (5) a discharge passageway.

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7. The servoid metering valve seconding to claim 6, wherein the metering guslict is configured to be able to them a substantially third-tight sliding seal with at least a portion of the scaling portion of the scaling portion of the scaling portion.

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- 17. An acrosed metering valve according to claim 16, wherein the polymer is selected from the group consisting of acetal, nylon, polyester, polybutylene terephilastate, polymetrylpentere, polyphenylenesuifide, polyeryletherketones, thermotropic liquid crystalline polymers, polypropylene, high density polypropylene, ethylenotetrylpene copolymer, poly-visylidene difluoride and mixtures thereof.
- 18. An aerosol metering valve according to obtim 17, wherein the polymer is selected from the group consisting of polymyletherhetones, thermotropic liquid crystalline polymers, polymethylpenines, polyphenylene sulfide and mixtures thereof.
- 19. An aerosol metering valve according to any one of claim 16 to 18, wherein the motoring gasket is made of a material comprising a thermoset elastomer selected from the group comisting of EPDM, nitrile, buryl subber, chloroburyl rubber, brumoburyl rubber and necessrone.
- A metered dose dispensing device comprising an aerosol metering valve according to any preceding claim.
- A meterod dose dispensing device according to claim 20, wherein said meterod
 dose dispensing device is a meterod dose inhaler.

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 As acrosol metering valve according to any preceding claim, wherein said angle of metering surface is equal to or greater than about 10°.

- As across metering valve according to any preceding claim, wherein said angle of
 metering surface is equal to or greater than about 20°.
 - 10. An acrosol metering valve according to any preceding of chaim, wherein said engine of metering surface is equal to or preser than about 10°.
- An across containing valve according to any preceding of claim, wherein said angle of motering surface is equal to or less than about \$0°.
 - 12. An across metering valve according to any proceeding of claim, wherein said engls of metering surface is equal to or less than about 70°.
 - An acrossi metering valve according to any preceding of claim, wherein said angle
 of metering surface is equal to or less than about 60°.
- An acrosol mozering valve according to any proceeding claim, wherein the metering surface comprises no eignificant portion aligned parallel or nearly parallel to the locaritadinal exis.
 - 15. An acrossol metering valve according to any preceding claim, wherein the metering gashet is co-modded with at least a portion of the valve stem.
 - 16. An acrosed motoring valve according to any proceeding claim, wherein the motoring gasket is made of a material comprising a thermophastic distincer or a thermoset clustomer and wherein the non-motoring-gasket portion of the valve stem is made of a material comprising a polymer.

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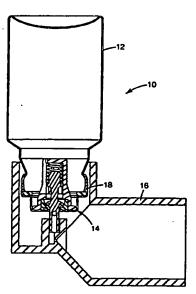
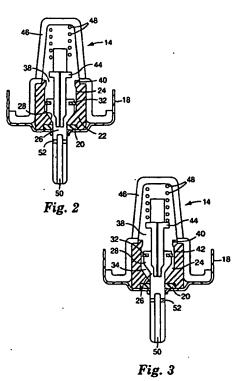
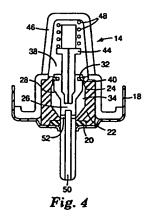


Fig. 1

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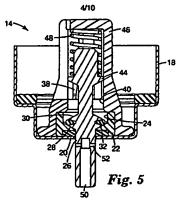


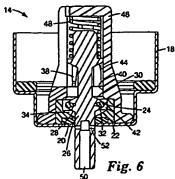
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WO 2004/022143

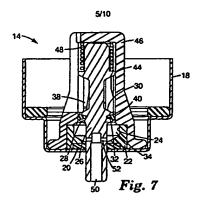
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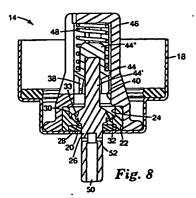




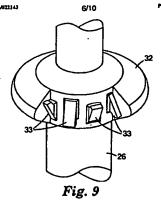
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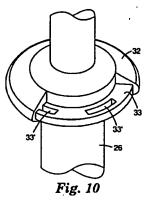
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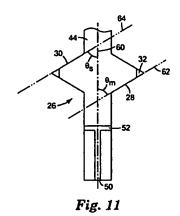




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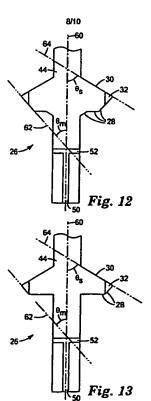


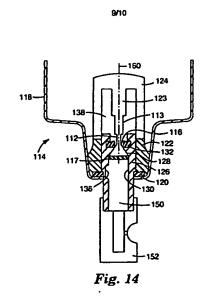
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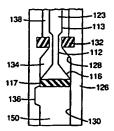


Fig. 15

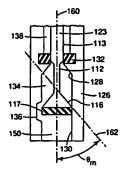


Fig. 16